

ARMY RESEARCH LABORATORY



Analyses of High Energy Plasma Capillaries for Use in Electrothermal- Chemical Launch

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1. INTRODUCTION

High energy electrical plasmas are of interest to the U.S. Army for application to the electrothermal-chemical (ETC) propulsion concept where their use can potentially increase the muzzle kinetic energy beyond that of a conventional gun, or it can provide a rapid and repeatable ignition source for conventional gun munitions. Much research has been reported over the years in the areas of ETC propulsion and the physics relating to plasmas that are characteristic of ETC guns.²⁻⁴ This report provides information from a recent study of ETC type plasma devices, in the form of theoretical calculations of plasma behavior during various operating conditions. The ETC plasma study includes the following:

- a. Analyses and interpretation of plasma properties including steady state resistance, exit pressure, and core temperature of the ETC plasma. Plasmas are assumed to be operating during freely expanding "choked flow" as well as "unchoked flow" conditions. The unchoked condition arises for some plasmas where a 450-megapascal (MPa) pressure boundary assumption is made;
- b. Plasma calculations are performed for three capillary geometries having various radii, and based on the results of the calculations, conclusions are drawn regarding the applicability of the different capillary dimensions for the various ETC propulsion concepts.

2. PLASMA MODEL ASSUMPTIONS

The plasma calculations undertaken here are performed with the steady state plasma model of John Powell from the U.S. Army Research Laboratory, the details of which have been reported previously in several technical publications (see References 1, 4). The code is used here with the following assumptions. First, the liner material of the plasma capillary is considered to be polyethylene. Although other materials can be used for capillary liners (e.g., peek glass, polycarbonate, etc.), polyethylene is considered a standard material whose behavior as a plasma-generating device is similar (with respect to plasma power dissipation, conductivity, and temperature) to that of devices constructed from other materials.⁵ In addition, the conductivity model implemented by the model is that of Kurilenkov-Valuev. The use of this conductivity model results in a modification of the Spitzer conductivity model used in the plasma code, by adjusting the collision frequency between electrons and ions at lower plasma temperatures. Although the use of the model is less frequent in recent plasma modeling work,⁶ the model has demonstrated good agreement with recent experimental plasma data.⁷ Finally, the calculated plasma temperatures are for the core or bulk plasma. The bulk temperatures predicted here take

into account a plasma surface temperature assumption which is known to cause somewhat higher bulk plasma temperatures and resistances with lower plasma exit pressures, compared to calculations being performed that assume a completely isothermal assumption. However, the plasma output parameters as a function of power and energy will generally behave the same. This can easily be verified by exercising the code during both conditions and comparing the output parameters.

2.1 Plasma Capillary Assumptions

For comparing plasma parameters such as resistance, pressure, and temperature, it was decided to examine plasma behavior at equivalent power and energy levels as opposed to electrical current level. This approach is desirable since two capillaries with different geometries, which are operating at identical input current, can produce plasmas that exhibit widely differing powers and total energies. Of course, because of the differences in capillary dimensions, the output parameters of interest (resistance, pressure, and temperature) will also exhibit great variation, regardless of an identical input current. As a result, it was decided to classify plasmas by power and energy level (based on an assumption of a 3-ms constant current input pulse) as opposed to the current level itself. An analysis can now be performed on plasmas (capillaries) having similar power and energy characteristics, which in general, are important criteria for determining the applicability to a given ETC concept.

For a given ETC concept, however, a range of input electrical energies will be required for proper implementation, depending upon which ETC approach is selected. The source of this electrical energy is, of course, the high energy electrical plasma. For example, for an ETC igniter, it is believed that less than 1 megajoule (MJ) of electrical energy over a period of several milliseconds will be required to properly ignite a 120-mm conventional propellant charge. This is based on simplified assumptions of energy content and discharge characteristics of standard benite primers presently used to ignite large caliber (120-mm) gun systems. On the other hand, for electrical enhancement of propellant burn rates or temperature compensation of conventional propellants, both of which could possibly result in enhanced gun performance, it is believed that a minimum of about 1 MJ of electrical plasma energy will be required for proper ETC gun operation.³

Three power levels, which are believed to be appropriate representatives of the requirements of the ETC concepts just described, were selected for this task. These include approximately 180 MW, 700 MW, and 1.8 gigawatts (GW). Given a time constant of 3 ms,

which should be a good representation of the electrical application time required for each of the ETC concepts considered, three energy levels of approximately 500 kJ, 2 MJ, and 5 MJ result, all of which fall within the range of energies that might be required for the ETC concepts just discussed.

For the remainder of the report, plasma properties are plotted with respect to total plasma energy, based on the approach just described. For each of the plots in Figures 1 through 6 of the following section, dividing the energy by the constant of 3 ms yields the plasma power amplitude for the calculation.

In addition, for the calculations performed here, the capillary lengths were fixed at 11.84 cm, which could realistically be used in a 120-mm tank cannon application. In addition, for simplicity, it was decided to investigate only three capillary radii. Again, the radii are selected for application to a 120-mm gun chamber and were chosen at 1.92 mm, 4.75 mm, and 7.0 mm. For the remainder of the report, the convention in referring to the capillaries is as follows: Capillary 1, 7.0-mm radius x 11.84-cm length; Capillary 2, 4.75-mm rad. x 11.84-cm length; and Capillary 3, 1.92-mm rad. x 11.84-cm length.

In the following section, calculations with the model are performed to determine the resistance, pressure, and temperature behavior of plasmas from three different capillaries, at each of the power and energy levels being considered. The first set of calculations has no boundary pressure, while the latter are performed with a 450-MPa boundary pressure. The convention in referring to the nominal plasma energy level assumed in the calculations is as follows: low, 0.5 MJ; medium, 2 MJ; and high energy level, 5 MJ.

2.2 Plasma Calculations

The steady state resistance, exit pressure, and plasma core temperature were selected as parameters of interest and included in the investigation. For each of the capillaries (1 through 3), an input current was chosen to give the approximate power and energy level required by the study. The choice of input current is the result of a somewhat arbitrary process in which the plasma code is exercised in an iterative manner, until the input current and plasma resistance values are such that the plasma power and energy levels are close enough to the preselected target values of power and energy. For this process, the steady state plasma power is determined from the product of the calculated plasma voltage drop (depending on the conductivity characteristics of the plasma) and the test current, at the given current level. The current is adjusted, either

increased or decreased, until the target power and energy levels are reasonably matched. For this study, reasonable agreement was considered agreement within about 18% of target values, although much better agreement could easily be obtained through further iteration with the code.

Since the plasma resistance plays a role in the transfer of electrical energy from a power supply to the plasma, the behavior of plasma resistance as a function of energy is investigated. For these calculations, unchoked flow is assumed by the model. The results are given in Figure 1, for each of the three capillaries at the given energy levels (low, medium, high), where the plasma resistance varies from about 13 milliohms ($m\Omega$) (Capillary 1 at high energy) to as much as 195 $m\Omega$ (Capillary 3 at low energy). Figure 1 demonstrates rather strong relationships among plasma resistance, operating energy, and capillary radius.

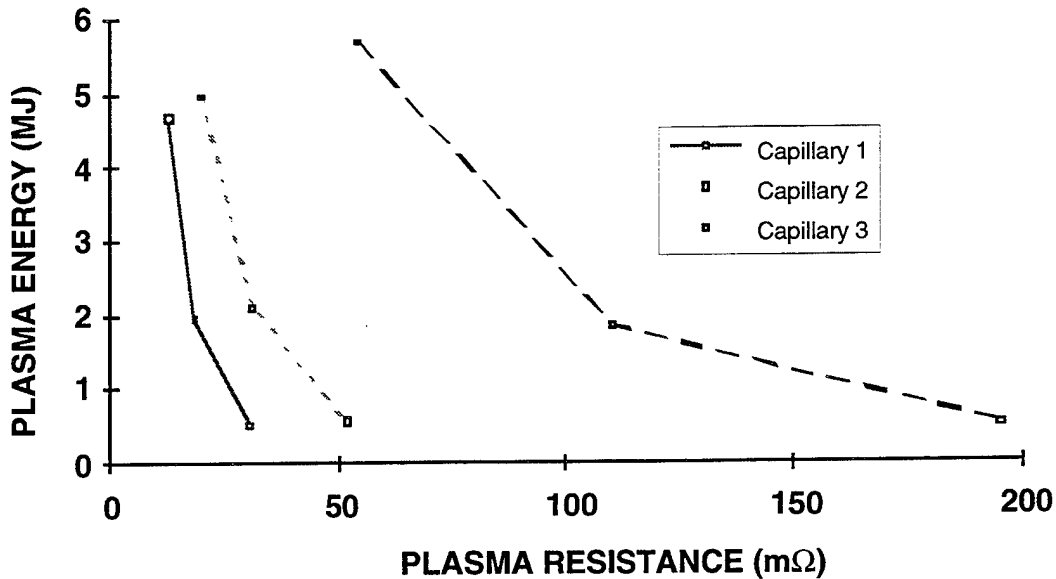


Figure 1. Plasma Energy Versus Resistance for Capillaries 1 Through 3, Having Radii as Depicted: 7.0, 4.75, and 1.92 mm, and Choked Flow Condition.

It is noticed how a very large dynamic range results for Capillary 3 (smallest diameter) resistance, over the given energy range, while the converse is true as the capillary radius is systematically increased.

Figures 2 and 3 are plots of plasma energy versus plasma exit pressure and plasma temperature, respectively. The exit pressure is the pressure at the open end of the capillary where plasma gases initially appear as the plasma flows from the capillary, while the plasma temperature is that experienced in the core of the plasma. Once again, it is noted how Capillary 3

has a wide (dynamic) range of exit pressures and core temperatures compared to Capillaries 1 and 2.

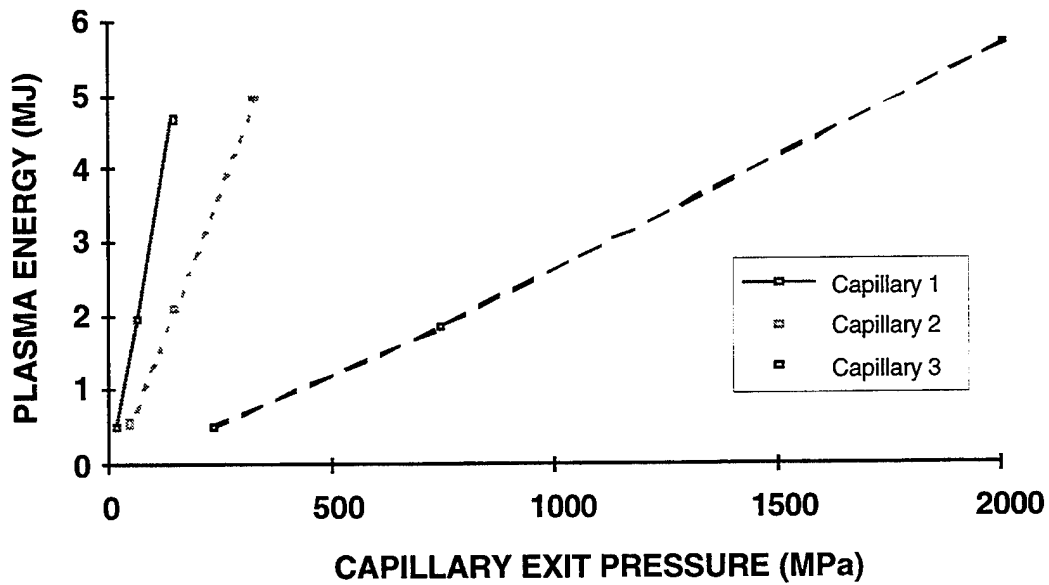


Figure 2. Plasma Energy Versus Exit Pressure for Capillaries 1 Through 3 Having Radii as Depicted, 7.0, 4.75, and 1.92 mm, and Choked Flow Condition.

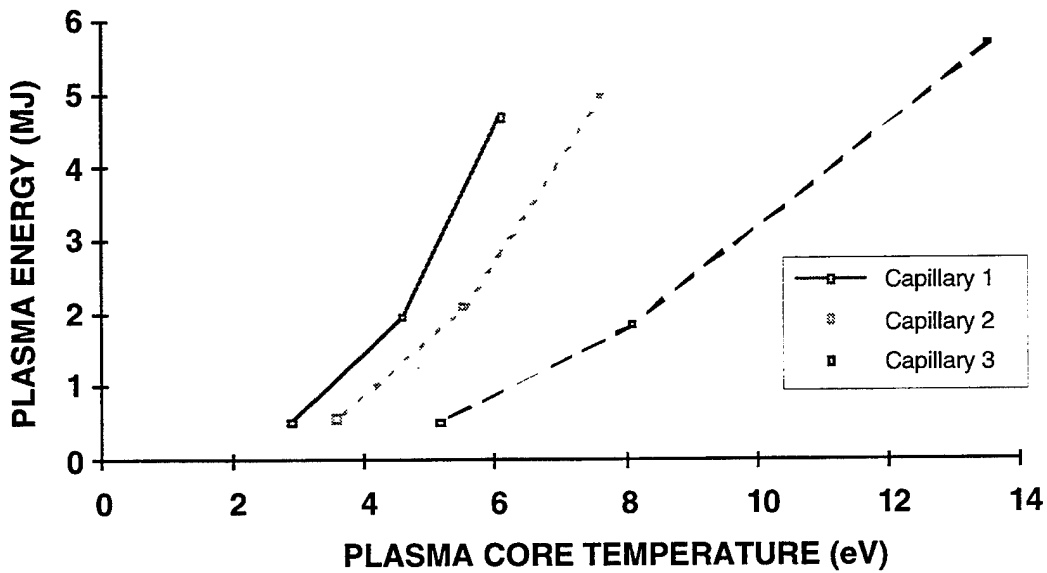


Figure 3. Plasma Energy Versus Core Temperature for Capillaries 1 Through 3 Having Radii as Depicted, 7.0, 4.75, and 1.92 mm, and Choked Flow Condition.

Figures 4 through 6 are the results of plasma calculations with the additional assumption of a pressure boundary condition at the plasma exiting plane. For this set of calculations, the boundary pressure is set at 450 MPa. The calculations are now performed only for Capillaries 2 and 3 with all previous calculation assumptions remaining unchanged. The results with the pressure boundary condition are plotted in Figures 4 through 6 (broken lines) together with the results from the previous calculations, which did not have the externally applied 450-MPa pressure boundary (solid lines). Figure 4 contains the plasma resistance relationships; Figure 5 contains the exit pressure relationships; and Figure 6 shows the core temperature relationships.

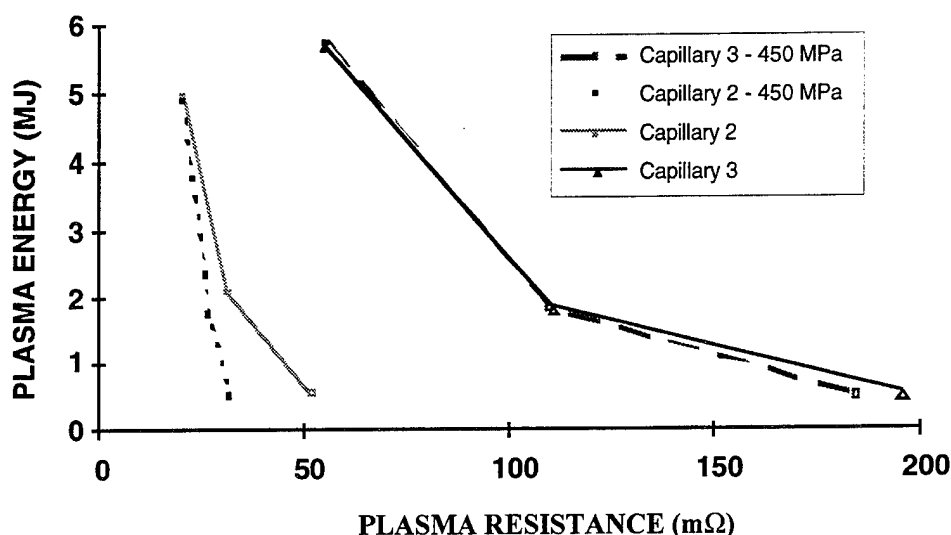


Figure 4. Plasma Energy Versus Resistance for Capillaries 2 and 3 Having Radii as Depicted, 7.0, 4.75, and 1.92 mm, and 450-MPa Pressure Boundary Condition.

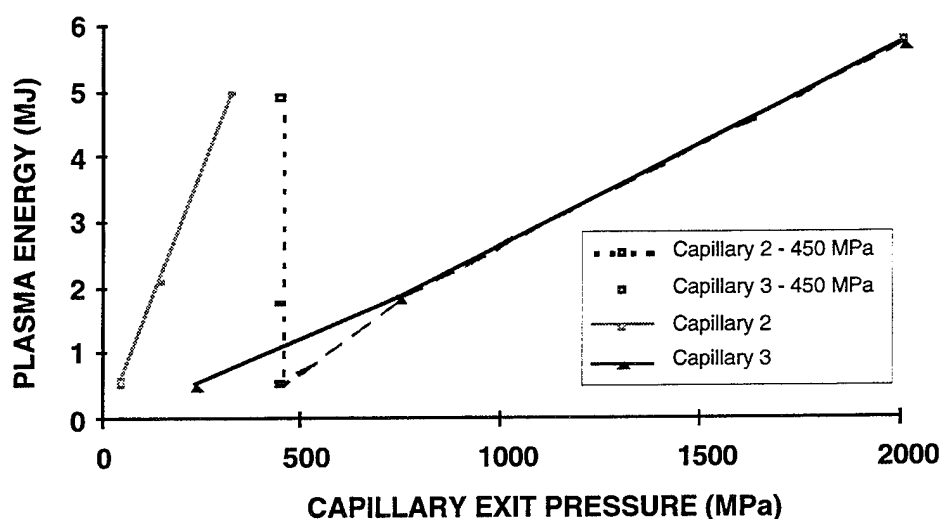


Figure 5. Plasma Energy Versus Pressure for Capillaries 2 and 3 Having Radii as Depicted, 7.0, 4.75, and 1.92 mm, and 450-MPa Pressure Boundary Condition.

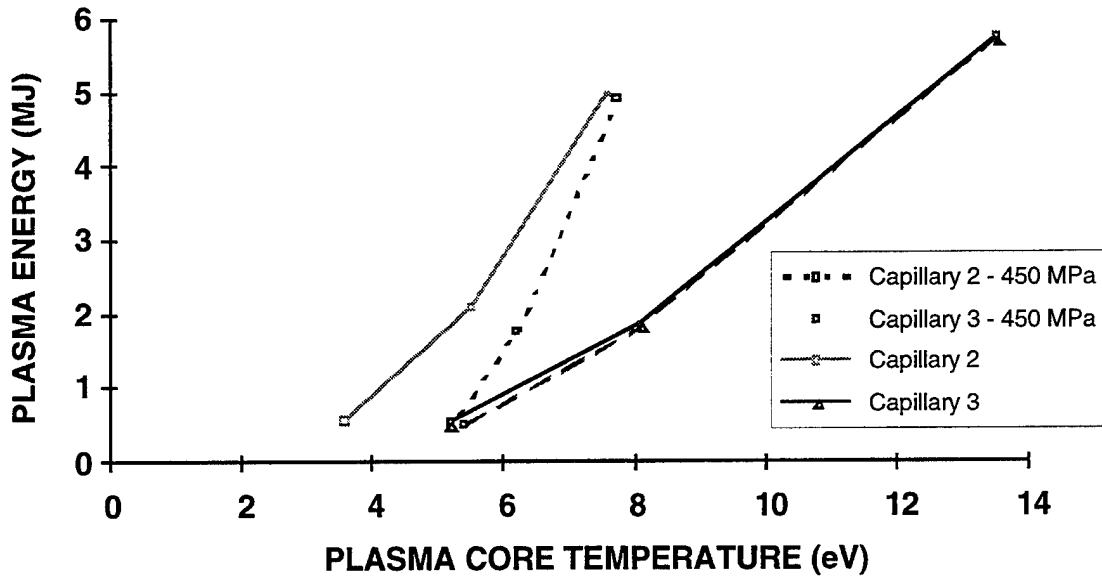


Figure 6. Plasma Energy Versus Temperature for Capillaries 2 and 3 Having Radii as Depicted, 7.0, 4.75, and 1.92 mm, with 450-MPa Pressure Boundary Condition.

3. DISCUSSION

The data for the calculations performed here are arranged in Tables 1 and 2. Table 1 gives the input parameters for the choked flow calculations along with the outputs for each capillary at the given energy and power levels. Table 2 shows the results for the calculation having the 450-MPa boundary condition for Capillaries 2 and 3 at each of the three energies and powers. Note that the numbers in Table 2 under the heading of percent difference represent the difference between choked and pressure boundary values, as a percentage. Percent difference as calculated here represents the absolute value of the choked value minus the pressure boundary value divided by the choked value.

For Capillary 2, the exit pressure is obviously dominated by the boundary pressure of 450 MPa, with increases of 406 (918%), 304 (208%), and 125 (39%) MPa for the low, medium, and high energies, respectively. The resulting temperatures are 5.2, 6.2, and 7.7 electron volts (eV), respectively, for the low, medium, and high energy levels. This represents an increase in temperature of 1.63 (44%), 0.7 (13%), and 0.13 (1.3%) eV, compared to the previous calculations without the 450-MPa boundary condition. The resistance of the Capillary 2 plasma is also sensitive to the pressure boundary, with decreases in resistance ranging from 20.4 m Ω (39%) to 0.3 m Ω (1.5%) over the range of energies investigated.

Table 1. Plasma Calculation Results for Capillaries 1 Through 3 During the Choked Flow Condition at Low, Medium, and High Energy and Power Levels

Capillary Dimensions (number)	Input Current (kA)	Plasma Resistance (mΩ)	Input Power (GW)	Input Energy (MJ)	Plasma Exit Pressure (MPa)	Plasma Core Temp (eV)
7.0 mm (1)	75	30.5	0.17	0.52	19.8	2.9
	187	18.6	0.65	1.96	64.0	4.6
	350	12.8	1.57	4.70	145.0	6.1
4.75 mm(2)	60	51.7	0.19	0.56	44.2	3.6
	150	31.2	0.70	2.10	146.0	5.5
	287	20.2	1.67	4.98	325.0	7.6
1.92 mm(3)	30	195.0	0.18	0.53	235.0	5.2
	75	110.0	0.62	1.86	744.0	8.1
	187	54.9	1.89	5.70	2000.0	13.5

Table 2. Plasma Calculation Results for Capillaries 2 and 3 During 450-MPa Pressure Boundary Condition at Low, Medium, and High Energy and Power Levels

Capillary Dimensions (number)	Input Current (kA)	Plasma Resistance (mΩ)		Input Power (GW)	Input Energy (MJ)	Plasma Exit Pressure (MPa)		Plasma Core Temp (eV)	
		Percent Δ				Percent Δ		Percent Δ	
4.75 mm(2)	75	31.3	39.5	0.18	0.53	450	918	5.2	44.4
	150	26.3	16	0.59	1.78	450	208	6.2	13
	287	19.9	1.5	1.64	4.92	450	39	7.7	1.3
1.92 mm(3)	30	184	5.6	0.17	0.49	450	92	5.4	3.8
	75	110	0	0.62	1.85	744	0	8.1	0
	187	54.9	0	1.92	5.80	2000	0	13.5	0

General observations for Capillaries 1 and 2 (larger diameters) include

- a. Plasma output parameters of resistance, pressure, and temperature are less sensitive to the input energy level assumed in the calculations, compared to Capillary 3 (smallest diameter).

b. Pressure boundary conditions have a strong influence over all plasma parameters considered in the study, at nearly every energy level. Resistance tends to drop, exit pressure increases, and core temperature increases for the plasmas of these capillaries, as the pressure boundary is applied to the calculation.

c. Lower exit pressures are experienced in nearly all calculations with these capillary dimensions (19.8 to 325 MPa). As a result, the ability for Capillaries 1 and 2 to inject plasma material into a pressurized gun chamber remains in question at the relatively low plasma pressures calculated. Larger capillaries might therefore be best used purely as an ignition source when plasma injection late in the ballistic cycle is not a requirement and when plasma output parameters with respect to input energy level are more stable.

The relationships for Capillary 3 are nearly unchanged by the added 450-MPa pressure boundary condition, regardless of energy level. In fact, for Capillary 3, the plasma resistance is identical for medium and high energies, while it is only decreased by 11 m Ω (5.6% difference) for the low energy case. The pressure and temperature of the plasma from Capillary 3 is increased by 215 MPa (91%) and 0.22 eV (3.8%), respectively, at low energy, and it remains completely unchanged in exit pressure and core temperature for medium and high energies. The output parameters of Capillary 3 are obviously dominated by the self-generated capillary pressure at all energies considered, especially medium and high, regardless of the 450-MPa pressure boundary condition. Based on these results, it seems reasonable that such a capillary would be appropriate for ETC propulsion concepts requiring continued plasma flow from the capillary into the gun chamber, during the ballistic cycle.

The summary of observations for Capillary 3 (small diameter) calculations includes the following:

a. Exit pressures and core temperatures increase more rapidly, compared to the other capillaries examined, as input energy is increased. The plasma resistance decreases more rapidly as input energy is increased.

b. The small diameter capillary is much less sensitive to pressure boundary conditions at the exit plane of the capillary, with respect to resistance, exit pressure, and core temperature, in comparison with other capillaries in the study. In fact, in some calculations, the output is completely unchanged by the pressure boundary, which indicates that the self-pressure of the plasma is dominant.

c. Exit pressures and core temperatures achieved extreme levels (2000 MPa, 13.5 eV) as the energy approached 5 MJ.

In summarizing this set of calculations, capillaries having diameters similar to those of Capillary 3 appear to be best for injection of plasma material into a pressurized gun chamber, perhaps late in the ballistic cycle. Of course, this may come at the expense of a very high core temperature and a somewhat higher plasma resistance and pressure. The use of smaller (diameter) capillaries for ETC performance augmentation will then require the ability to employ higher temperature plasmas as well as employ pulsed power supplies of higher impedances, although the latter of these should not be difficult. In addition, the ability to use plasmas with widely fluctuating output parameters must be considered, if a variety of energy levels is needed for proper ETC operation. This is because of the large dynamic range observed for each of the plasma output parameters (resistance, pressure, temperature) as a function of input energy.

The large dynamic range observed in Capillary 3 may have practical limitations if relied upon in an ETC application. For example, it has been shown in previous investigations that the electrical transfer efficiency of a fixed impedance pulsed power supply will exhibit a poor (approximately 40%) electrical transfer efficiency for capillaries having a resistance unmatched to that of the power supply.⁷ As a result, one might expect that a fixed impedance power supply will have a large variation in transfer efficiency with small diameter capillaries, over a given range of input power and energy levels. Large capillary plasmas could therefore be described as more stable in terms of their impedance behavior and transfer efficiencies with respect to power and energy input levels. One technical method of overcoming variations in transfer efficiency is to allow the impedance of the power supply to fluctuate with the plasma resistance. This, of course, could translate into a more complex power supply in terms of the additional switching and control components that are necessary to achieve the more dynamic power supply.

Additional computations and experiments for the purpose of further defining the behavior of plasmas at energy levels and of dimensions appropriate for ETC applications should be pursued aggressively before final conclusions are drawn with regard to optimal ETC plasma capillaries. The calculations in this report are performed with potentially severely limiting assumptions (e.g., one-dimensionality, isothermal effects, exclusion of hydrodynamics effects). As a result, it is highly advisable to continue theoretical and experimental exercises in the areas of ETC plasma investigations, with increasing levels of complexity before making any serious or profound conclusions with regard to ETC plasma capillary selection.

4. SUMMARY AND CONCLUSIONS

Theoretical calculations have been performed with a one-dimensional, steady state, isothermal plasma model with the objective of defining high energy plasma output parameters of interest to the electrothermal propulsion concept. Capillary radii were varied over a range of 1.92 to 7.00 mm, while the input current level was modulated between 30 kA and 350 kA for capillaries having a fixed length of 11.84 cm. The range of plasma powers and energies investigated include 0.17 to 1.89 GW and 0.52 to 5.70 MJ, respectively. The plasma output parameters of resistance, exit pressure, and core temperature fluctuated greatly over the range of energy and capillary diameters used. The range of resistance, pressure, and temperature is 12.8 to 195 m Ω , 19.8 to 2000 MPa, and 2.9 to 13.5 eV, respectively. The effect of a 450-MPa external pressure boundary condition was noticed to have a more significant impact on the plasma output parameters for large diameter capillaries and little or no impact on small diameter capillaries.

Large diameter capillaries studied here (Capillaries 1 and 2) showed a reduced sensitivity to the plasma energy level with respect to output parameters (resistance, pressure, temperature). An externally applied pressure boundary condition (450 MPa) had a strong influence on plasma output parameters, and the self-generated plasma pressures experience were generally much less than those of the small capillary (Capillary 3). Based on these observations, it appeared that a larger capillary might best be used in the application of an ETC igniter.

The small diameter capillary (3) was observed to have output parameters that were much more sensitive to the plasma energy level used; it was much less sensitive to the externally applied (450-MPa) pressure boundary condition, and it produced very large exit pressures and core temperatures. As a result, it might appear that a smaller diameter capillary would be best for applications when injection of electrical plasma energy into a gun chamber for a longer period in the ballistic cycle, such as ETC performance augmentation, is a requirement.

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REFERENCES

1. Powell, J. D., and Zielinski, A. E., "Theory and Experiment for an Ablating-Capillary Discharge and Application to Electrothermal-Chemical Guns," BRL-TR-3355, U.S. Army Ballistic Research Laboratory, Aberdeen Proving Ground, MD, June 1992.
2. Oberle, W., Stobie, I., DelGuercio, M., White, K., Bourham, M., Gilligan, J., "Summary of Experimental Efforts to Determine Plasma-Augmented Burn Rates for Solid Propellants," U.S. Army Research Laboratory and North Carolina State University, ARL-TR-782, Aberdeen Proving Ground, MD, June 1995.
3. White, K. J., Oberle, W. F., Juhasz, A. A., Stobie, I. C., Nekula, K., Katulka, G. L., Driesen, S., "Electrothermal-Chemical Propulsion with High Loading Density Charges," U.S. Army Research Laboratory Technical Report, ARL-TR-845, Aberdeen Proving Ground, MD, August 1995.
4. Powell, J. D., "Analysis of Piccolo-Type Injectors for Electrothermal-Chemical Launch," U.S. Army Research Laboratory Technical Report, ARL-TR-952, Aberdeen Proving Ground, MD, January 1996.
5. Batteh, J., Powell, J., Sink, D., Thornhill, L., "A Methodology for Computing Thermodynamic and Transport Properties of Plasma Mixtures in ETC Injectors," IEEE Transactions of Magnetism, Vol., 31, No. 1, January 1995.
6. Powell, J. D., Private communication, U.S. Army Research Laboratory, March 1996.
7. Princeton Combustion Research Laboratories, "Final Report: A Time Dependent, Lumped Parameter Power-Plasma-Interior-Ballistic Code (PPIB) for Electrothermal-Chemical (ETC) Gun Performance Prediction," Delivered under contract to the U.S. Army Research Laboratory, Aberdeen Proving Ground, MD 21005-5066, June 1995.
8. Katulka, G., Oberle, W., Wren, G., Okamitsu, J., Messina, N., "Pulse-Power, Plasma, and Interior Ballistic Simulations for Application to Electrothermal-Chemical Guns," Technical Report ARL-TR-1070, U.S. Army Research Laboratory, Aberdeen Proving Ground, MD 21005-5066, March 1996.

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USARO
ATTN TECH LIB D MANN
PO BOX 12211
RSCH TRI PK NC 27709-2211

1 COMMANDER
USABRDEC
ATTN STRBE WC TECH LIB VAULT
BLDG 315
FT BELVOIR VA 22060-5606

1 COMMANDER
USA TRAC FT LEE
DEFENSE LOGISTICS STUDIES
FT LEE VA 23801-6140

NO. OF
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1 PRESIDENT
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 FT SILL OK 73503

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 USACGSC
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 USASWS
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 FT BRAGG NC 28307

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 ATTN SMCRA QA HI LIBRARY
 RADFORD VA 24141

1 COMMANDANT
 USAFAS
 ATTN STSF TSM CN
 FT SILL OK 73505-5600

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 ATN SFAE SD HVL
 D LIANOS
 PO BOX 1500
 HUNTSVILLE AL 35887-8801

3 COMMANDER
 USA FSTC
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 C BEITER
 220 SEVENTH ST NE
 CHARLOTTESVILLE VA 22901

1 COMMANDANT
 USA FACS
 ATTN ATSF CO MW
 B WILLIS
 FT SILL OK 73503

1 OFC NAVAL RSCH
 ATTN CODE 473 R S MILLER
 800 N QUINCY ST
 ARLINGTON VA 22217

2 COMMANDER
 NSSC
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 SEA 64
 WASHINGTON DC 20362-5101

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 C GOTZMER
 SLVR SPRNG MD 20902-5000

2 COMMANDER
 NSWC
 ATTN CODE R13 K KIM
 CODE R13 R BERNECKER
 SLVR SPRNG MD 20902-5000

3 CDR NSWC INDIAN HEAD DIV
 ATTN 6210 C SMITH
 6210J K RICE
 6210C S PETERS
 INDIAN HEAD MD 20640-5035

3 CDR NSWC DAHLGREN DIV
 ATTN CODE G33 T DORAN
 J COPLEY
 CODE G30 G&M DIV
 DAHLGREN VA 2448-5000

3 CDR NSWC DAHLGREN DIV
 ATTN CODE G301 D WILSON
 CODE G32 GUNS SYSTEMS DIV
 CODE E23 TECH LIB
 DAHLGREN VA 2448-5000

1 CDR NSWC CRANE DIV
 ATTN CODE 4052 S BACKER
 BLDG 108
 CRANE IN 47522-5000

2 CDR NUSC ENG CONV DEPT
 ATTN CODE 5B331 R S LAZAR
 TECH LIB
 NEWPORT RI 02840

1 CDR NSWC INDIAN HD DIV
 ATTN CODE 270P1 MR E CHAN
 101 STRAUS AVE
 INDIAN HEAD MD 20640

NO. OF
COPIES ORGANIZATION

1 CDR NSWC INDIAN HD DIV
ATTN CODE 3120 MR R RAST
101 STRAUS AVE
INDIAN HEAD MD 20640

1 CDR NSWC INDIAN HD DIV
ATTN CODE 210P1 R SIMMONS
101 STRAUS AVE
INDIAN HEAD MD 20640

2 CDR NSWC INDIAN HD DIV
ATTN CODE 6210 S BOYLES
N ALMEYDA
101 STRAUS AVE
INDIAN HEAD MD 20640

1 CDR NAWC
ATTN CODE 3891 A ATWOOD
CHINA LAKE CA 93555

1 CDR USAARDEC
ATTN SMCAR CCH J HEDDERICH
BLDG 1
PCTNY ARNSL NJ 07806-5000

1 OLAC PL TSTL
ATTN D SHIPLETT
EDWARD AFB CA 93523-5000

10 CIA
OFC OF CENTRAL REFERENCE
DISSEMINATION BRANCH
RM GE47 HQS
WASHINGTON DC 20502

1 CIA
ATTN J E BACKOFEN
HQ RM 5F22
WASHINGTON DC 20505

3 DIRECTOR LANL
ATTN B KASWHIA
H DAVIS
E526 W REASS
LOS ALAMOS NM 87545

1 DIRE LLNL
ATTN MS L355 A BUCKINGHAM
PO BOX 808
LIVERMORE CA 94550

NO. OF
COPIES ORGANIZATION

1 DIR SANDIA NAT LAB
COMBUSTION RSCH FACILITY
ATTN R ARMSTRONG
DIV 8357
LIVERMORE CA 94551-0469

1 DIR SANDIA NAT LAB
COMBUSTION RSCH FACILITY
ATTNS VOSEN
DIV 8357
LIVERMORE CA 94551-0469

1 UNIVERSITY OF ILLINOIS
DEPT OF MECH INDUST ENGR
ATTN PROF H KRIER 144 MEB
1206 N GREEN ST
URBANA IL 61801

1 JHU CPIA
ATTN T CHRISTIAN
10630 LTLE PATUXENT PKWY
STE 202
COLUMBIA MD 21044-3200

2 PENN STATE UNIV
DEPT OF MECHANICAL ENGR
ATTN J BROWN
312 MECHANICAL ENGR BLDG
UNIVERSITY PK PA 16802

1 NCSU
ATTN J G GILLIGAN
BOX 7909
1110 BURLINGTON ENGR LABS
RALEIGH NC 27695-7909

1 NCSU
ATTN M BOURHAM
BOX 7909
1110 BURLINGTON ENGR LABS
RALEIGH NC 27695-7909

2 INST FOR ADV TECH
ATTN DR H FAIR
P SULLIVAN
4030 2 W BAKER LANE
AUSTIN TX 78759-5329

1 INST FOR ADV TECH
ATTN DR I MCNAB
4030 2 W BAKER LANE
AUSTIN TX 78759-5329

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COPIES ORGANIZATION

1 SRI INTERNATIONAL
PROPULSION SCIENCE DIV
ATTN TECH LIB
333 RAVENSWOOD AVE
MENLO PARK CA 94025

1 SPARTA
ATTN DR M HOLLAND
945 TOWNE CENTER DR
SAN DIEGO CA 92121-1964

2 UNITED DEFENSE
ATTN MR M SEALE
DR A GIOVANETTI
4800 E RIVER RD
MINNEAPOLIS MN 55421-1498

1 UNITED DEFENSE
ATTN MR J DYVIK
4800 E RIVER RD
MINNEAPOLIS MN 55421-1498

1 HERCULES INC
RADFORD ARMY AMMO PLANT
ATTN D A WORRELL
PO BOX 1
RADFORD VA 24141

1 HERCULES INC
RADFORD ARMY AMMO PLANT
ATTN E SANFORD
PO BOX 1
RADFORD VA 24141

2 GDLS
ATTN MR F LUNSFORD
DR M WEIDNER
PO BOX 2074
WARREN MI 48090-2074

2 OLIN ORDNANCE
ATTN V MCDONALD LIBRARY
H MCELROY
PO BOX 222
ST MARKS FL 32355

1 OLIN ORDNANCE
ATTN D WORTHINGTON
PO BOX 222
ST MARKS FL 32355

1 PAUL GOUGH ASSOC INC
ATTN P S GOUGH
1048 SOUTH ST
PORTSMOUTH NH 03801-5423

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COPIES ORGANIZATION

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ATTN H W WAMPLER
PO BOX 5010
SAN LEANDRO CA 94577-0599

1 ROCKWELL INTL
ROCKETDYNE DIV
ATTN BA08 J E FLANAGAN
6633 CANOGA AVE
CANOGA PK CA 91304

1 ROCKWELL INTL
ROCKETDYNE DIV
ATTN BA08 J GRAY
6633 CANOGA AVE
CANOGA PK CA 91304

1 SCIENCE APPLICATIONS INC
ATTN J BATTEH
1225 JOHNSON FERRY RD
STE 100
MARIETTA GA 30068

1 SCIENCE APPLICATIONS INC
ATTN L THORNHILL
1225 JOHNSON FERRY RD
STE 100
MARIETTA GA 30068

1 ELI FREEDMAN & ASSOC
ATTN E FREEDMAN
2411 DIANA RD
BALTIMORE MD 21209

1 VERITAY TECH INC
ATTN MR E FISHER
4845 MILLERSPORT HWY
E AMHERST NY 14051-0305

1 BATTELLE
ATTN TACTEC LIB
J N HUGGINS
505 KING AVE
COLUMBUS OH 43201-2693

1 CA INSTITUTE OF TECH
JET PROPULSION LAB
ATNT L D STRAND MS125 224
4800 OAK GROVE DR
PASADENA CA 91109

NO. OF
COPIES ORGANIZATION

1 CA INSTITUTE OF TECH
JET PROPULSION LAB
ATTN D ELLIOT
4800 OAK GROVE DR
PASADENA CA 91109

1 USA BENET LAB
ATTN SMCAR CCB R
DR DR S SPOCK
WATERVLIET NY 12189

1 MARTIN MARIETTA DEFENSE SYS
ATTN DR J MANDZY
MAIL DROP 42 220
100 PLASTICS AVE
PITTSFIELD MA 01201

1 STATE U OF NY
DEPT OF ELEC ENGR
ATTN DR W J SARGEANT
BONNER HALL RM 312
BUFFALO NY 14260

1 TEXAS TECH UNIVERSITY
DEPT OF EE COMPUTER SCIENCE
ATTN DR M KRISTIANSEN
LUBBOCK TX 79409-4439

1 UNIV OF TEXAS AT ARLINGTON
DEPT OF ELEC ENGR
ATT DR L GORDON
BOX 19016
ARLINGTON TX 76019-0016

1 WILKES UNIVERSITY
DEPT OF ELEC ENGR
ATTN DR A ARMAND
WILKES BARRE PA 18766

2 UNIVERSITY OF DELAWARE
DEPT OF ELEC ENGR
ATTN DR N GALLAGHER
DR J KOLODZEY
NEWARK DE 19716

1 COLORADO SCHOOL OF MINES
DEPT OF ENGINEERING
ATTN C BRAUN
GOLDEN CO 80401

1 SNL
ATTN MR M GRUBELICH
DIV 2515
PO BOX 5800
ALBUQUERQUE NM 87185

NO. OF
COPIES ORGANIZATION

2 LOCKHEED MARTIN DEF SYSTEMS
PRINCETON COMBUSTION RSCH LABS
ATTN N A MESSINA
11 DEER PARK DR BLDG IV SUITE 119
MONMOUTH JUNCTION NJ 08852

1 COMMANDER USA ARDEC
ATTN SFAC ASM TMA AS
R BILLINGTON
PICATINNY ARSENAL NJ 07806-5000

2 RARDE
GS2 DIVISION BLDG R31
ATTN DR C WOODLEY, DR G COOK
FORT HALSTEAD
SEVENOAKS KENT TN14 7BP
ENGLAND

1 MATERIALS RESEARCH LABORATORY
SALISBURY BRANCH
ATTN ANNA WILDEGGER GAISSMAIER
EXPLOSIVES ORDNANCE DIVISION
SALISBURY
SOUTH AUSTRALIA 5108

ABERDEEN PROVING GROUND

5 DIR ARL
ATTN AMSRL OP AP L (TECH LIB)
BLDG 305 APG

5 CDR USAATC
ATTN WALTON
G RICE
D LACEY
C HERUD
STECs DA ID
L FRANCIS

36 DIR USARL
ATTN AMSRL WT I MAY
J ROCCHIO
D ECCLESHALL
AMSRL WT P A HORST
E SCHMIDT
P KASTE
AMSRL WT PC B FORCHE
R PESCE-RODRIGUEZ
AMSRL WT PB P PLOSTINS
D LYON
A ZIELINSKI
AMSRL WT PD B BURNS
AMSRL WT PA T MINOR
M DEL GUERCIO
J DESPIRITO

NO. OF
COPIES ORGANIZATION

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 J KNAPTON
 G KATULKA (5 CYS)
 G KELLER
 P CONROY
 D KOOKER
 W OBERLE
 C RUTH
 T ROSENBERGER
 I STOBIE
 P TRAN
 K WHITE
 G WREN
 M MCQUAID
 AMSRL WT T W MORRISON
 AMSRL WT W C MURPHY
 AMSRL WT WB W D'AMICO
 AMSRL WT WD
 A NILER
 C HOLLANDSWORTH
 J POWELL